NONINVASIVE EVALUATION OF THE ELASTICITY OF COMMON CAROTID ARTERY WALL

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The elasticity of common carotid arteries was examined on the basis of noninvasive ultrasonic measurements of the diameter of the carotid artery and the systolic and diastolic pressures as determined by a cuff on the brachial artery. The measurements were performed for a group of 20 males, aged from 27 to 45 years. The examinees were fighter plane pilots. The examinations were carried out for different systolic and diastolic pressures which were recorded along with measurements of the diameter of the carotid artery during rest, following an exercise test. This paper presents the results of measurements of the maximum and minimum diameters of the common carotid artery for different systolic and diastolic pressures in the brachial artery. Good coincidence was gained between the experimental results and the logarithmic function as described by POWAŁOWSKI. The coefficient of the determination \( R^2 \) fell between 0.993 and 0.999.

On the basis of the results of the measurements of the artery diameter and the blood pressure, the values of coefficients describing the elastic properties of the common carotid arteries were defined. The investigated coefficients included: the elastic modulus \( E_p \), the arterial distensibility coefficient \( DC \), the cross-sectional compliance \( CC \) and the logarithmic stiffness coefficient \( \alpha \).

KEY WORDS:
Arterial wall elasticity, carotid artery, ultrasound

1. Introduction

The evaluation of the elasticity of arteries was based on the examination of changes in the transversal dimensions of the vessel which are caused by blood pressure variations. It involves differently defined coefficients which are often applied in references to characterise the elastic properties of arterial walls. E.g., they include:

1) the elastic modulus \( E_p \) as described by PETERSON in 1960 [14]:

\[
E_p = \frac{\Delta P}{D_0} \frac{D}{\Delta D} ,
\]

where \( \Delta D/D_0 \) is a relative increase in the vessel diameter as a function of the blood pressure growth \( \Delta P \).
2) the arterial distensibility coefficient $DC$ and the cross-sectional compliance $CC$ as applied in 1986 by Reneman et al. in carotid wall studies [19, 20]:

$$DC = \frac{2 \Delta D / Dd}{\Delta P}, \quad (1.2)$$

$$CC = \frac{\pi \Delta D \cdot Dd}{2 \Delta P}. \quad (1.3)$$

Experimental studies performed on large arterial vessels (the aorta, the carotid artery, and the femoral artery) by Berge [3], Loon [9], Simon [22] and Hayashi [6] demonstrated that there is a nonlinear dependence between the change in the transversal artery dimensions and that in the blood pressure. This means that the coefficients described by formulae (1.1)–(1.3) depend on the blood pressure, making it difficult the comparatively evaluate the arterial wall elasticity studies performed on their basis.

So far there has been no unambiguous agreement on the form of the analytical dependence between the blood pressure and the change in the transversal arterial dimensions. Most of the functions proposed in the references are empirical in nature. They include the functions described by Loon [9], Hayashi [6], Stettler [23], Meister [11], Langehouwerst [8] and Powałowski [15, 16, 17]. Out of these functions, it is only the one proposed by Powałowski that can be determined via noninvasive measurements of systolic and diastolic blood pressures and the maximum and minimum vessel diameters. It has the following form:

$$D^2 (P) = Dd^2 \left[ 1 + \frac{1}{\alpha} \ln \frac{P}{Pd} \right], \quad (1.4)$$

where $\alpha$ is defined as the logarithmic coefficient of arterial wall stiffness, in the following form:

$$\alpha = \frac{Dd^2}{D_s^2 - Dd^2} \ln \left( \frac{P_s}{Pd} \right), \quad (1.5)$$

where $D_s$ and $Dd$ are vessel diameters for the systolic pressure $P_s$ and the diastolic pressure $Pd$, respectively.

The coefficient $\alpha$ proposed by Powałowski is an attempt to take into account the effect of the blood pressure on the stiffness coefficient in comparative examinations. The coefficients described by formulae (1.1)–(1.3) and (1.5) are applied in evaluating the elasticity of arterial walls in noninvasive studies [1, 17, 19, 20]. In these studies, the ultrasonic method is used to determine the maximum and minimum arterial diameters. Cuff-measured systolic and diastolic pressures are subordinated to the above values. As the common carotid arteries are examined, the blood pressure is measured with a cuff on the brachial artery of a patient in a lying position.
The purpose of the work is to examine ultrasonically the dependence between the maximum and minimum diameters of the common carotid artery and the blood pressure in the brachial artery as well as to analyse the coefficients $E_p$, $DC$, $CC$ and $\alpha$ for different blood pressures.

2. The results of research and discussion

The examinations were carried out on the common carotid arteries of a group of 20 men, aged from 27 to 45. The patients were fighter plane pilots. (The study was performed at the Military Institute of Aviation Medicine in Warsaw).

The examinations were performed using the measuring system, called the Vascular Echo Doppler, elaborated by the present authors. Its block diagram is shown in fig. 1. The equipment consisted of a pulsed ultrasound system tracking displacements of carotid artery walls. The accuracy of arterial wall displacement identification was 7 $\mu$m. The internal artery diameter was determined on the basis of digital measurements of the time between selected echo slopes detected from the internal layer of the arterial wall [5, 18].

Fig. 1. A block diagram of the measuring system: A/D — an analog-to-digital converter; FIFO — memory (First Input, First Output) applied for collecting echo image data.

The frequency of the transmitted ultrasound was 6.75 MHz. The ultrasound was focused at the 1 – 3 cm depth from the surface of the skin. The width of the ultrasound beam at the focus was 1 mm (defined for the sound pressure of $-20$ dB compared with the maximum value on the beam axis). The width of the transmitted pulsed ultrasound was 0.3 $\mu$s (2 cycles of a high-frequency transmitter), representing its length of 0.45 mm in tissue. As an effect, it was possible to gain single echoes from the external and internal surfaces of the walls of the common carotid artery under study.
To facilitate the location of the artery under study in the course of the measurements, the pulse probe was mechanically coupled with that of a c.w. Doppler flowmeter. The pulse probe was set perpendicular to the artery, assuming as the measure of perpendicular position the gaining of the maximum amplitude of echoes from the blood vessel walls.

In the course of the evaluation, the measured data were displayed on the screen of an IBM PC connected on-line with an ultrasound system and memorized by this computer (Fig. 2). Along with the ultrasonically measured data, the values of the systolic and diastolic pressures which were cuff-measured were entered into the computer’s memory.

The measurements were performed on a lying patient before and after exercise. The exercise examinations were carried out on a cyclometer. Directly following the exercise, the high blood pressure gradually dropped during rest, to reach after 8—10 minutes the pressure measured before the exercise test.

![Graphs](image)

**Fig. 2.** The data presented in the course of the measurement on the monitor of an IBM PC: a) echoes from the walls of the common carotid artery, b) internal artery diameter, c) artery diameter variations (scale 0.5 mm), d) blood flow velocity; psys and pdia are the systolic and diastolic blood pressures (mm Hg) in the brachial artery.
The pressure was measured every minute. The pressures between the successive measuring points were calculated using linear interpolation. The intervals of systolic and diastolic pressures measured for particular examines are shown in Table 1. Changes in the systolic pressure were greater than those in the diastolic pressure, falling between 14 mmHg and 60 mmHg.

Table 1. The results of measurements of the systolic \( P_s \) and the diastolic \( P_d \) brachial blood pressures and the diameter \( D \) of the common carotid arteries in patients: \( R^2 \) — the coefficient of determination calculated for the evaluation of the degree of approximation of the results of experimental research using the logarithmic function \( D(P) \) (formula (1.4)) \( D \text{ min}_x \) — the mean value of the minimum diameter

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Examples of the distributions obtained for the experimental points (the relations between the artery diameter \( D \) and the blood pressure \( P \)) for systolic and diastolic pressures are shown in Fig. 3.

The distribution of the experimental points was described using the logarithmic function \( D(P) \) as obtained from formula (1.4). The coefficient of determination \( R^2 \) for the group of the people examined fell within the interval between 0.993 and 0.999 (see Table 1). The scatter of the majority of the experimental points round the theoretical curve fell in the interval of values corresponding to error of roughly \( \pm 14 \) \( \mu \)m as the change in the vascular diameter was measured.

The high coincidence between the results of the studies and the logarithmic function as described by Powalowski indicates that the latter function can be adopted as the basis for the evaluation of the elasticity of common carotid arteries performed
Fig. 3. The results of measurements of the dependence between the diameter $D$ of the common carotid artery and the blood pressure $P$ in the brachial artery for three patients numbered 9, 10 and 16 (compare Tables 1 and 2). The maximum and minimum carotid diameters were subordinated respectively to the systolic and diastolic pressures. The solid line represents the logarithmic function $D(P)$ determined from formula (1.4). The figure shows the mean values of the stiffness coefficients $\alpha$ (formula (1.5)) calculated for patients as well as the coefficient of determination $R^2$ calculated for the evaluation of the degree of approximation of the experimental research results as a function of the logarithmic function $D(P)$.

on the basis of measurements of the maximum and minimum diameters of the carotid artery and the systolic and diastolic pressures as measured in the brachial artery.

The logarithmic function $D^2(P)$ is an empirical one, which, as its author [17] showed, corresponds with good accuracy ($R^2 = 0.9868$) to the results of examinations performed directly in the carotid artery over the pressure range from 25 mmHg to 200 mmHg.

Assuming for the common carotid artery the values of the systolic and diastolic pressures determined in the brachial artery, it is necessary to discuss this type of comparative evaluation. The pressure wave which propagates along the vascular system changes its shape. As Mc Donald [10] noticed, in moving from the aorta towards the lower-lying peripheral vessels, the systolic pressure is observed to increase as the diastolic and mean pressures drop slightly. There have been, e.g.,
attempts to explain this phenomenon with the effect of summation of the progressive and reflected pressure waves. Thus, the question arises whether a similar phenomenon takes place in the case of vessels in the upper part of the body and what are the possible blood pressure differences between the aorta and the brachial artery. The common carotid artery is very close to the aortic arch, and it can be assumed that the blood pressure difference between these vascular points can be neglected.

In 1955, in examining the blood pressure when using a catheter simultaneously in the brachial artery and the aortic arch, Kroeker [7] observed that for the same heart work cycle the systolic pressure in the brachial artery was 9% greater, and the diastolic pressure was 4% lower than the analogous pressures in the aorta. Some doubts have on the other hand been raised by the fact that when measuring in a similar way the blood pressures in the radial and femoral arteries this author obtained for all of the three arteries almost the same blood pressure differences between them and the aortic arch. Referring, in turn, to the experimental work performed by Arndt [2], Riley [21] noted that the pressure difference between the common carotid artery and the brachial artery can be neglected. A very significant argument for this view is provided by the research results presented in 1982 by Borow [4]. They apply to comparative evaluation between the blood pressure in the brachial artery determined noninvasively by the oscillographic method (the automatic cuff method) and the blood pressure measured using a catheter in the ascending aorta. These studies, carried out on a group of 30 persons aged from 30 to 83 years, indicated that for a lying patient the differences in the systolic and diastolic pressures between the aorta and the brachial artery are 1% and 1.7% (the mean value), respectively, so they can be neglected in practice.

In the light of the research mentioned, it should be said that the method applied for the evaluation of the systolic and diastolic pressures in the common carotid artery as based on measurements of these pressures in the brachial artery should not introduce significant error into the noninvasive examination of the elasticity of the carotid arteries.

On the basis of the studies performed, in keeping with formulae (1.1) - (1.3) and (1.5), the values of the coefficients $E_p$, $DC$, $CC$ and $\alpha$ were determined. The mean values of the coefficients and the relative changes in their values are shown in Table 2. These results indicate that the relative changes in the value of the coefficient $\alpha$ are several times smaller than the changes in the values of the other coefficients. Figs. 4 - 7 represent the relative (with respect to the mean value) values of particular coefficients as a function of the systolic pressure. They indicate that the value of the coefficient $\alpha$ does not depend significantly on the systolic pressure but the pressure has a distinct impact on the values of the coefficients $E_p$, $DC$ and $CC$. The coefficient $E_p$ increases, whereas the coefficients $DC$ and $CC$ decrease as a function of the systolic pressure.

The effect of the diastolic pressure on the values of the coefficients under study which describe the elastic properties of arteries is difficult to identify in an experimental way, because the diastolic pressure changes in the patients examined were slight. Assuming as the starting point of discussion the previously considered
Fig. 4. The relative (with respect to the mean value of $\alpha_p$) value of the logarithmic stiffness coefficient $\alpha$ as a function of variations in the systolic pressure $P_s$ as calculated from examinations of a 39-year-old man (no. 11, see Tables 1 and 2). The correlation coefficient is 0.167.

Fig. 5. The relative (with respect to the mean value of $E_{p_0}$) value of the elastic module $E_p$ as a function of variations in the systolic pressure $P_s$ calculated on the basis of examinations performed on a 39-year-old man (No. 11, see Tables 1 and 2). The correlation coefficient is 0.946.

[458]
Fig. 6. The relative (with respect to the mean value of \( DC_0 \)) value of the arterial distensibility coefficient \( DC \) as a function of variations in the systolic pressure \( Ps \) calculated from examinations of a 39-year-old man (No. 11, see Tables 1 and 2). The correlation coefficient is \(-0.937\).

Fig. 7. The relative (with respect to the mean value of \( CC_0 \)) cross-sectional compliance \( CC \) as a function of variations in the systolic pressure \( Ps \) calculated on the basis of examinations performed on a 39-year-old man (No. 11, see Tables 1 and 2). The correlation coefficient is \(-0.944\).
logarithmic function between the square of the vessel diameter and the blood pressure, it should be said that the diastolic pressure affects the values of all the elasticity coefficients under study. In the case of the stiffness coefficient $\alpha$,

\[
\text{for } Pd = Pn \quad \alpha = \alpha_n, \quad (2.1)_1
\]

\[
\text{for } Pd < Pn \quad \alpha = \alpha_n - \ln \left(\frac{Pn}{Pd}\right), \quad (2.1)_2
\]

\[
\text{for } Pd > Pn \quad \alpha = \alpha_n + \ln \left(\frac{Pd}{Pn}\right), \quad (2.1)_3
\]

where $Pn$ is the pressure $Pd$ at the reference point.

It results from formulae (2.1) that the effect of the diastolic pressure on the value of the coefficient grows smaller when the value of the coefficient $\alpha$ increases.

The evaluation of the effect of the blood pressure on the values of the particular elasticity coefficients is significant in comparative studies. An example of such studies in the references is the search for a correlation between the arterial elasticity and the age of patients [1, 12, 13, 17, 19, 20].
3. Conclusions

It is difficult to verify the noninvasively assessed for the evaluation of the elasticity of common carotid artery by the proposed logarithmic function, the ultimate results of the measurements of the elasticity coefficients. They include the function between the blood pressure and the age in the transversal diameter of the common carotid artery, a) the relation between the systolic and diastolic pressures in the common carotid artery and the brachial artery, c) the accuracy of the brachial blood-pressure measurement using cuff, d) the accuracy of femoral artery diameter measurements using ultrasound. Instead of an analysis of particular factors, the authors proposed a comprehensive evaluation. It consisted in the statistical measurements of the elasticity of the common carotid artery for different blood pressures and in investigating the relation between the diameter of the common carotid artery and the blood pressure measurement in the brachial artery.

The results of the measurements and calculations indicate that:

1) The distribution of points: the artery diameter - the blood pressure could be correlated with high accuracy by the proposed logarithmic function, as described by formula (1.4). The coefficient of determination $R^2$ varied between 0.95 and 0.999 (Table 1). The scatter of most experimental points is around the theoretical curve fall in

Fig. 9. The elastic modulus $E_p$ determined for common carotid arteries as a function of the age of patients. The solid line represents the linear regression function (Table 3).

[461]
Fig. 10. The arterial distensibility coefficient $DC$ determined for common carotid arteries as a function of the age of patients. The solid line represents the linear regression function (Table 3).

Fig. 11. The cross-sectional compliance $CC$ determined for common carotid arteries as a function of the age of patients. The solid line represents the linear regression function (Table 3).
Figures 8—11 show the values of particular coefficients as a function of age. Linear regression was applied in analysing this dependence. For the group of the persons examined it is only the stiffness coefficient $\alpha$ that correlates significantly ($p<0.05$) with age (Table 3). As was demonstrated previously, the value of this coefficient do not depend on systolic blood pressure variations in the course of the examination.

**Table 3.** The coefficients describing the linear regression function $(ax+b)$ for dependencies between the values of $\alpha$, $E_p$, $DC$ and $CC$ and the age of patients; $r$ — the correlation coefficient

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<td>$CC$</td>
<td>-0.0730</td>
<td>10.8113</td>
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</table>

### 3. Conclusions

It is difficult to verify the noninvasive method for the evaluation of the elasticity of common carotid arteries because of the many factors which affect the ultimate result of measurements of the elasticity coefficients. They include: a) the function between the blood pressure and a change in the transversal dimensions of the common carotid artery; b) the relation between the systolic and diastolic pressures in the common carotid artery and the brachial artery; c) the accuracy of the brachial blood pressure measurement using cuff; d) the accuracy of acrorid artery diameter measurements using ultrasound. Instead of an analysis of particular factors the authors proposed a comprehensive evaluation. It consisted in ultrasonic measurements of the diameter of the common carotid artery for different blood pressures and in investigating the relation between the diameter of the common carotid artery and the blood pressure measured in the brachial artery.

The results of the measurements and calculations indicate that:

1) The distribution of points: the artery diameter - the blood pressure could be represented with high accuracy by the proposed logarithmic function described by formula (1.4). The coefficient of determination $R^2$ varied between 0.993 and 0.999 (Table 1). The scatter of most experimental points round the theoretical curve fell in the interval of values corresponding to an error of roughly $\pm 14\,\mu m$ in the measurement of vessel diameter changes.

2) The effect of the systolic pressure on the value of the logarithmic stiffness coefficient $\alpha$ (formula (1.5)) can be neglected. The calculations were carried out for a group of 20 persons for whom the systolic pressures fell between 112 mmHg and 190 mmHg, and the systolic pressure variations came between 14 mmHg and
60 mmHg (Table 1). The relative changes in the value of the coefficient $\alpha$ as a function of the systolic pressure in patients never exceeded 10% (Table 2 and fig. 4).

3) The logarithmic stiffness coefficient $\alpha$ is a more objective indicator of the mechanical properties of the wall of the common carotid artery than the parameters used so far, including the elastic modulus $E_p$, the arterial distensibility coefficient $DC$ or the compliance $CC$. Its value does not change significantly as a function of the systolic pressure when the value of the coefficient $E_p$ grows as a function of the systolic pressure and the values of the coefficients $DC$ and $CC$ decrease as a function of that pressure (Figs. 4–7). The relative changes in the values of the coefficients $E_p$, $DC$ and $CC$ as a function of variations in the systolic pressure were from 1.2 to 5.1 times larger than the changes of the value of the logarithmic stiffness coefficient $\alpha$.

References


1. Introduction

The design principles of transducers with matching layers was described in the previous paper [5]. In this work the influence of electrical parameters, compensating inductances, a coaxial cable, wire connectors, a parallel resistance and input impedances of a transmitter and a receiver on the reflected pulse is discussed.

Calculations are carried out, modified Mason’s model described in [4] being assumed (Fig. 1). Because in this paper only the PZT ceramic transducers are discussed, the mechanical and dielectric losses can be neglected. All quantities are relative (dimensionless).

- frequency $\nu = \frac{f}{f_0}$
- mechanical impedance of the investigated medium $R_m = R_p / R_s$
- mechanical impedences of the matching layers $R_{M1} = R_p / R_{m1}$
- $R_{M2} = R_s / R_{m2}$